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A Simulation Approach for Investigating the Effect of Valeric Acid Concentration on Poly(3-hydroxybutyrate-co-3hydroxyvalerate) Generation in Presence of Methane

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Polyhydroxyalkanoates (PHAs) are biobased and biodegradable polymers that may be considered to replace fossil-based materials. However, their widespread deployment is slowed down because of the high production cost and their low quality. Using methane during the generation of poly(3-hydroxybutyrate-co-3-hydroxyvalerate) (PHB-co-HV) could reduce the production costs, which are usually owed to the carbon source used, and enhance the performance of the material. In fact, the properties of PHB-co-HV make it more suitable than the most common homopolymer, named poly(3-hydroxybutyrate) (PHB), for many applications since it is more flexible, has a wider thermal processing range, a lower crystallinity and permeability to water. In this work, the production of Poly(3-hydroxybutyrate-co-3-hydroxyvalerate) was simulated using an innovative process scheme consisting of two bioreactors working in series equipped with a gas recycling unit, which was designed to increase the methane mass transfer from the gas to the liquid. During the first step, a Methylocystis dominated culture was grown on ammonia and methane to reach a high cell concentration; then, the cells were moved to the second bioreactor and subjected to nutrients starvation to favour the metabolic pathway addressed to the accumulation of PHB-co-HV. The effect of the variation of valeric acid concentration (100-400 ppm), which was used as co-substrate, on the fraction of PHB-co-HV stored in the cells and the percentage of 3-hydroxyvalerate (3-HV) was investigated: results showed that the highest the valeric acid concentration, the lower the total polymer content and the higher the HV fraction accumulated.

1. Introduction

Bio-based and biodegradable plastics such as polyhydroxyalkanoates (PHAs) show several advantages over conventional petroleum-based materials, but their industrial diffusion is limited by their high production costs due to the carbonaceous substrate, fermentation procedures, yields on the selected substrate and extraction/purification process (Abate et al., 2022). It was reported that in 2004 the price of commercial polyhydroxyalkanoates was 15-17 times higher than that of conventional plastics, thus resulting in no-marketable. Many efforts have been made to meet the economic feasibility, and several studies today address the achievement of high levels of PHAs as a percentage of dry cell weight, improved fermentation conditions, low-cost recovery methods, low-cost substrates, high productivity in terms of grams of product per unit volume and the scalability of the process (Sipkema et al., 1998).

One valid approach to reduce the costs is the production of PHAs by mixed microbial cultures (MMC) since MMC require a lower sterility degree and basic equipment in comparison with monoseptic cultures (Policastro et al., 2021). Anyway, PHAs production by MMC has never been implemented at an industrial scale, where only pure cultures (wild or genetically modified strains) are used (Madison and Huisman, 1999). Moreover, it has

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Property	РНВ	Poly(3HB-co-HV)	PP
M [10 ⁵ g/mol]	1-8	3	2.2-7
ρ [kg/dm³]	1.25	1.2	0.905
Melting point [°C]	171-182	75-172	176
Crystallinity [%]	80	55-70	70
Glass transition temperature [°C]	5-10	-13-8	-10
O ₂ -permeability [cm/m ² kPa day]	0.4	n.d.	17
UV-resistance	Good	Good	Bad
Resistance to solvents	Bad	Bad	Good
Tensile strength [MPa]	40	25-30	38
Elongation to break [%]	6	8-1200	400
Young's modulus	3.5	2.9 (3%HV); 0.7 (25%3HV)	1.7
Biodegradability	Yes	Yes	No

2. Simulation strategy

The process to produce PHB-co-HV was simulated in *AspenPlus* using two reactors with a working volume of 1 m³, in which the liquid represented the batch charge and a gas stream containing methane was diffused continuously in the form of small bubbles ($d_b \approx 10$ mm) at a superficial gas velocity (U_g) of 0.02 ms⁻¹. A gas recirculation unit operating at a recycling ratio (RR) of 5, i.e. the ratio between the recycled flow rate and the initial fresh gas fed, was also implemented (Figure 1).



Figure 1: Main simulation flowsheet

178

The strategy implemented in this work consisted of the growth of a mixed Type II-dominated methanotrophic culture (Step I), followed by the accumulation of the polymeric granules into the cells under nutrient starvation (Step II). Since the yield of the process depends on biomass metabolism and the transfer rate of oxygen and methane to the liquid phase, both the kinetic constant and the gas-liquid mass transfer coefficients were estimated.

2.1 Biomass growth

During the growth of the mixed methanotrophic culture, an ammonia-based mineral salt medium was used, and a gas stream containing methane and oxygen (1:2 v/v%) was fed to the reactor (Table 1). The temperature was set at 27 °C and pressure at 1 bar; the duration of the process was assumed to be 96 h.

Growth reactor	GBIOMASS-IN	LBIOMASS-IN	GBIOMASS-OUT	LBIOMASS-OUT
G _{biomass} -out	CH4, O2	Mineral salt medium containing an initial concentration of the mixed methanotrophic consortium	CH4, O2, CO2	Mineral salt medium containing the grown biomass

Table 2: Description of the growth unit streams.

In these conditions, ammonia, methane and oxygen are converted to CO_2 and biomass ($C_5H_7NO_2$), according to the reaction proposed by Rostkowski et al. (2013) (Eq.1).

$$\frac{1}{4}CH_4 + \left(\frac{1}{4} + \frac{f_e}{4}\right)O_2 + \frac{f_s}{23}HCO_3 + \frac{f_s}{23}NH_4^+ \left(\frac{24}{23}f_s + f_e - 1\right)H^+ \rightarrow \left(\frac{1}{4} - \frac{4f_s}{23}\right)CO_2 + \left(\frac{f_e}{2} + \frac{9f_s}{23}\right)H_2O + \left(\frac{f_s}{23}\right)C_5H_7O_2N$$
(1)

In Eq.1, the degree of conversion depends on the partition coefficients f_e and f_s , which represent the fractions of electrons employed for reducing oxygen to water and cell synthesis, respectively. The values used in this work are those reported for a *Methylocystis*-dominated culture and account for 0.27 and 0.73, respectively. Moreover, since the growth of this strain was reported to be linear in time, the reaction kinetics was assumed a zero-order type, and the kinetic constant calculated was 0.000106 kmol m⁻³h⁻¹.

2.2 PHB-co-HV accumulation from methane

During the production of PHB-co-HV, a nitrogen-deprived mineral salt medium was considered, and a gas stream containing methane and oxygen (1:2 v/v) was fed to the reactor (Table 2), which was operated at 27 °C and 1 bar for 96 h. Valeric acid at 100 and 400 ppm was supplemented as a co-substrate to promote the formation of 3-HV monomers.

Accumulation reactor	G _{PHB-co-HV} -in	 Lpнв-co-нv -in	GPHB-co-HV-OUt	Lрнв-со-нv -out
G _{PHB-co-HV} -out L _{PHB-co-HV} -out G _{PHB-co-HV} -out	CH4, O2	Nutrient-deprived medium containing the grown biomass, valeric acid (100, 400 ppm)	CH4, O2, CO2	Nutrient deprived medium containing biomass rich in PHB-co-HV

Table 3: Description of the accumulation unit streams.

In the reaction considered, methane and oxygen are consumed by the biomass to produce CO_2 and the polymer (C₄H₆O₂).

$$\frac{1}{4}CH_4 + \left(\frac{1}{4} + \frac{f_e}{4}\right)O_2 \rightarrow \left(\frac{1}{4} - \frac{4f_s}{18}\right)CO_2 + \left(\frac{f_e}{2} + \frac{f_s}{3}\right)H_2O + \left(\frac{f_s}{18}\right)C_4H_6O_2$$

$$\tag{2}$$

The partition coefficients used were measured experimentally for a *Methylocystis*-dominated culture in the same conditions simulated (low and high valeric acid, methane as substrate). As for the growth phase, the kinetic constant was extrapolated from the literature, considering a zero-order reaction. Table 4 reports the kinetic and transfer data used for these simulations, which were calculated according to Amabile et al. (2022a).

Table 4: kinetic and transfer parameters used to simulate PHB-co-HV accumulation.

Parameter	Valeric acid [ppm]		
	100	400	
k _{kin} [kmol m ⁻³ h ⁻¹]	1.10x10 ⁻⁴	6x10⁻⁵	
fe	0.35	0.45	
fs	0.65	0.55	
kLa [s ⁻¹]	1x10 ⁻²	1x10 ⁻²	

3. Results

The results of the simulations, expressed in terms of production as a function of the time of biomass and PHBco-HV, are shown in Figure 2. The initial biomass content was 1 kg and reached 2.76 kg after 96 h of fermentation, while the amounts of biopolymer produced at the end of the cycle were 1.38 (33.3% of the total suspended solids) and 0.764 kg (18.7% of the total suspended solids) for the lower and higher valeric acid concentration, respectively. Despite the lower amounts of PHB-co-HV produced at 400ppm, the fraction of the 3-HV monomers was higher (40%mol). Similar results were previously reported in the literature (Myung et al., 2015), thus confirming the validity of the model implemented (Amabile et al., 2022c). Furthermore, other experimental works demonstrated the reduction of the polymer production obtained with high valeric acid concentrations, probably because of the lower pH values encountered in these cases (López et al., 2018).



Figure 2: Time course of the production of biomass and PHB-co-HV at low and high valerate concentrations

Other parameters used as performance indicators, such as the productivity of PHB-co-HV (pPHB-co-HV), the production of polymer for the unit of biomass (*PHB-co-HV/biomass*) and methane fed (*PHB-co-HV/CH*₄), are shown in Table 5.

180

Table 5: Results of the simulations for the two conditions studied: 100 and 400 ppm of valerate.

Parameter	Valeric acid [ppm]	
	100	400
<i>pPHB-co-HV</i> [g m ⁻³ d ⁻¹]	6.9	5.83
PHB-co-HV/biomass [g g ⁻¹]	0.499	0.23
PHB-co-HV/CH4 [g g ⁻¹]	0.155	0.13

The results show that when adding 100 ppm of valeric acid, the production of PHB-co-HV with respect to the initial biomass and the productivity of the polymer is higher than when supplying 400 ppm. These findings agree with the literature, where in the range 100-400ppm of valerate, the lower limit led to the highest production and 400ppm to the maximum HV content. Moreover, the productions here obtained for 1 m³ of working volume were higher than those reported in prior studies, where lower reactor capacities were considered (García-Pérez et al., 2018). As regards the production for the unit of methane, there is no significant difference between the two cases examined, thus indicating that the parameter depends on the mass transfer conditions, which in turn are related to the process and reactor design. In this context, it was previously demonstrated through simulations analysis that increasing the reactor volume enhances productivity but lowers the production related to methane consumption (Amabile et al., 2022b). These results suggest that alternative strategies to boost the mass transfer of methane and oxygen to the liquid phase should be evaluated when using larger volumes to improve the biopolymer production in bioreactors at larger scales. In this context, also other scale-up aspects, such as the study of the reactor geometry, the reduction of sterility conditions and the possibility of using low-cost substrates, should be evaluated.

4. Conclusions

The process to produce PHB-co-HV from methane was simulated in *AspenPlus*. A mixed microbial methanotrophic strain was used since it requires low sterility and could be a valuable option to reduce production costs. Two bubble column bioreactors with 1 m³ of working volume were implemented to perform the growth phase and the accumulation step. This latter was conducted with the addition of valeric acid as a co-substrate, which was fed at low (100 ppm) and high (400 ppm) concentrations in order to understand if the mass loss of PHB-co-HV at 400ppm could be compensated by the highest HV fraction. The results show that all the concentrations in the range 100-400ppm of valerate could be taken into account for PHB-co-HV production. The addition of low amounts of valeric acid does not modify the microbial activity, thus allowing the incorporation of 3-HV monomers without threatening the total production yields. On the other hand, a higher amount of valerate can inhibit microbial activity, thus inducing the formation of 3-HV granules but reducing the amount of polymer produced at the end of the cycle.

Nomenclature

 $\begin{array}{l} d_b - bubbles \ diameter \ [mm] \\ kla - gas-liquid \ volumetric \ mass \ tranfer \ coefficient \ [s^{-1}] \\ PHB - \ Poly(3-hydroxybutyrate) \\ PHB-co-HV - \ Poly(3-hydroxybutyrate-co-3-hydroxyvalerate) \\ M - \ molecular \ mass \ [g \ mol^{-1}] \\ \rho - \ density \ [kg \ m^{-3}] \\ 3-HV - \ 3-hydroxyvalerate \\ p-PHB-co-HV - \ volumetric \ productivity \ per \ day \\ U_g - \ superficial \ gas \ velocity \ [m \ s^{-1}] \end{array}$

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182